

SIMULATION AND EXPERIMENTAL VALIDATION FOR BETA HEAT TREATMENT OF URANIUM ROD BY DIRECT HEATING METHOD

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CONFERENCE**
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Outline

- ▣ Introduction
- ▣ Current method and drawbacks
- ▣ Direct heating method
- ▣ Mathematical analysis
- ▣ Numerical solution
- ▣ Experimental validation
- ▣ Conclusion
- ▣ References

Introduction

Uranium Phases

α :- 20 to 665 DegC

β :-665 to 776 DegC

γ :-776 to 1132 DegC

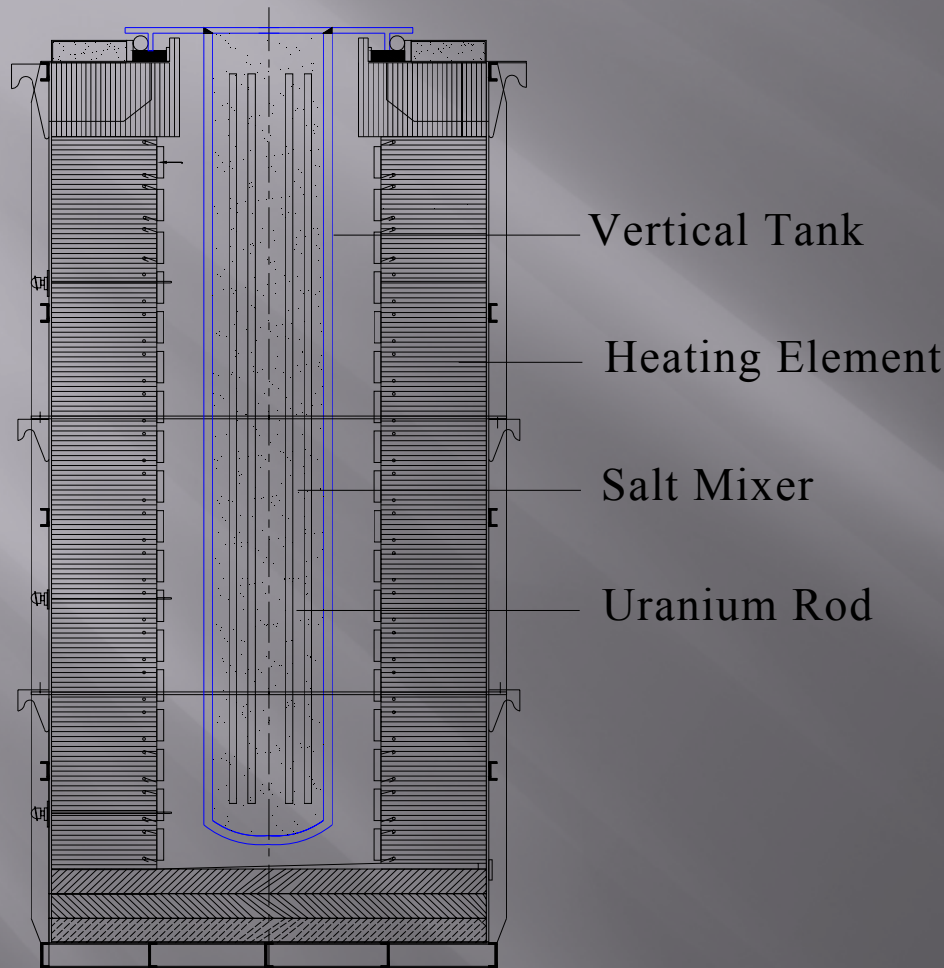
β heat treatment

Ur rods are heated upto 740 deg C and quench into water tank.

Purpose

To randomize the grains developed during rolling or extrusion.

Current method and drawbacks



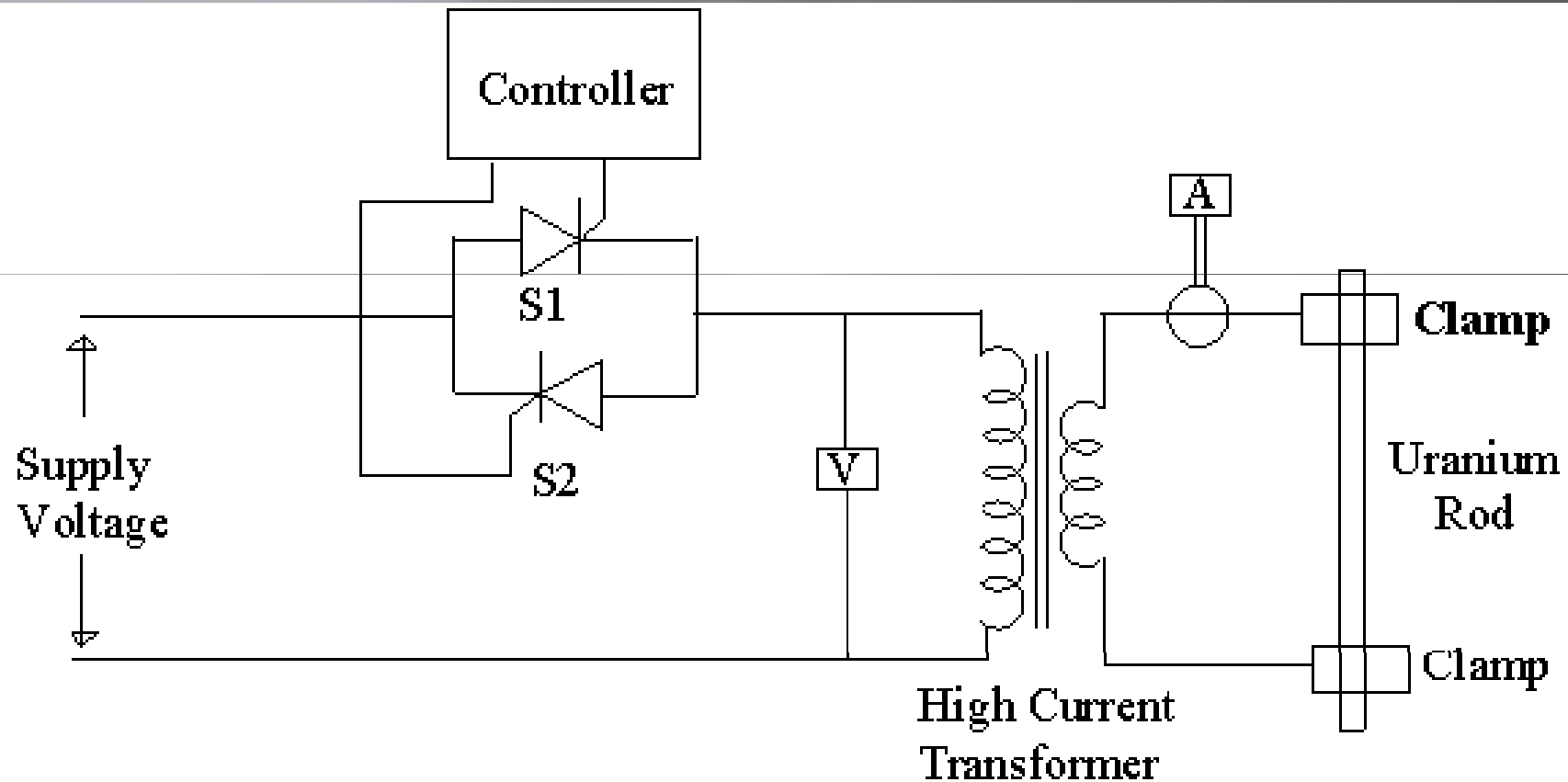
SALT BATH FURNACE

- 1.5 T Slat mixture
- (barium chloride-55 %, Sodium chlorides -25 %, potassium chloride- 20 %)

Drawbacks :-

- Low efficiency
- manual Handling of molten salt (> 600 deg C)
- Batch wise production.

Direct heating method



Mathematical analysis

- ▣ Coupled field problem.

Electric field

Heat transfer

- ▣ Electric field

Laplace equation $\nabla \cdot (\sigma(T) \nabla V) = 0$

Heat source term $Q = \sigma(T) (\nabla V)^2$

- ▣ Heat transfer

$$\nabla \cdot k \nabla T + Q = \rho c \frac{\partial T}{\partial t}$$

Phase change analysis

- ▣ Effective heat capacity
- ▣ Enthalpy method
- ▣ Heat Source method

$$\rho C_{eff}(T) \frac{\partial T}{\partial t} = \nabla(k \nabla T)$$

$$C_{eff} = \rho c_{\alpha} \quad (T < T_{\alpha})$$

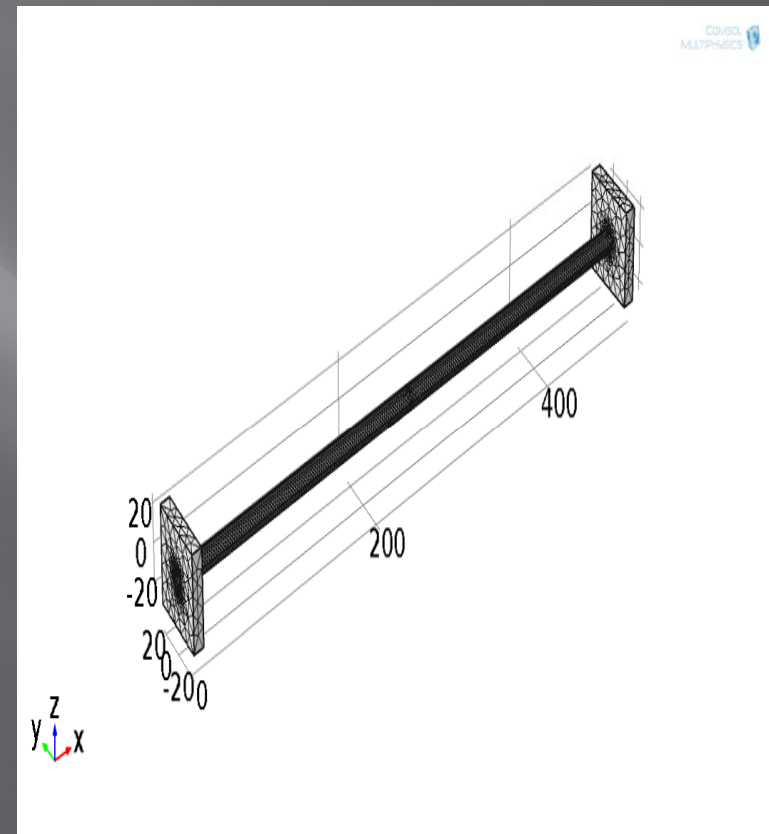
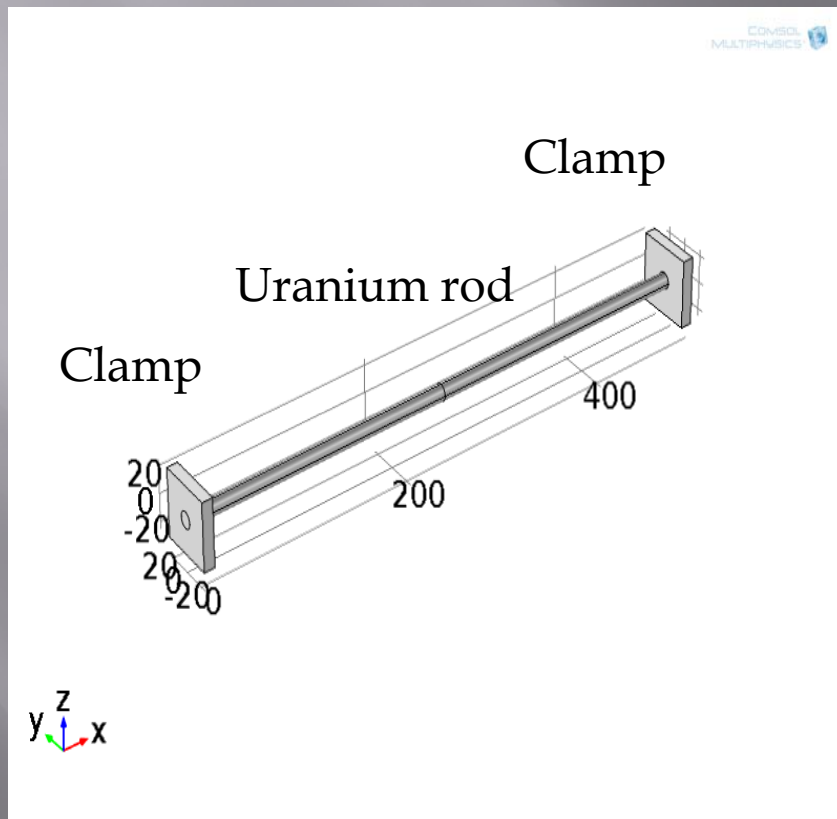
$$C_{eff} = \rho c_{\alpha-\beta} + \frac{L}{T_{\beta} - T_{\alpha}} \quad (T_{\alpha} \leq T \leq T_{\beta})$$

$$C_{eff} = \rho c_{\beta} \quad (T > T_{\beta})$$

COMSOL Multiphysics software

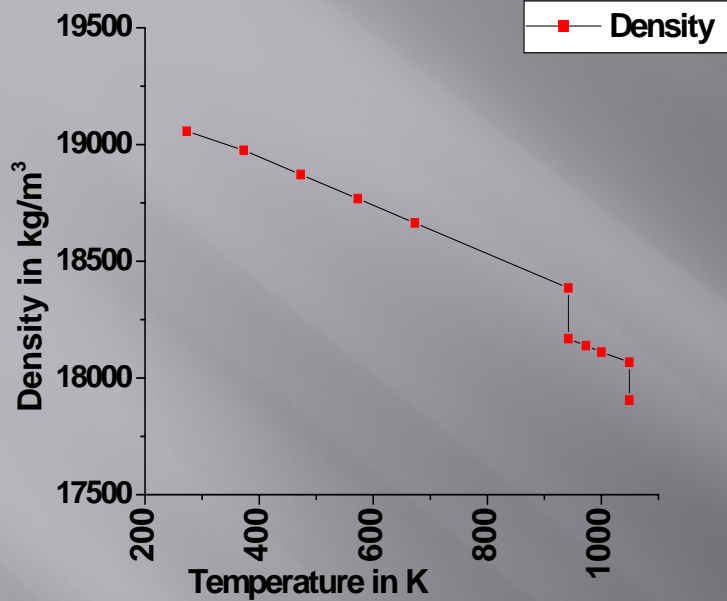
- ▣ Joule heating module.
- ▣ FEM based multiphysics software.
- ▣ Easy programming and analysis
- ▣ Phase change analysis is done by effective heat capacity method

Geometry and meshing

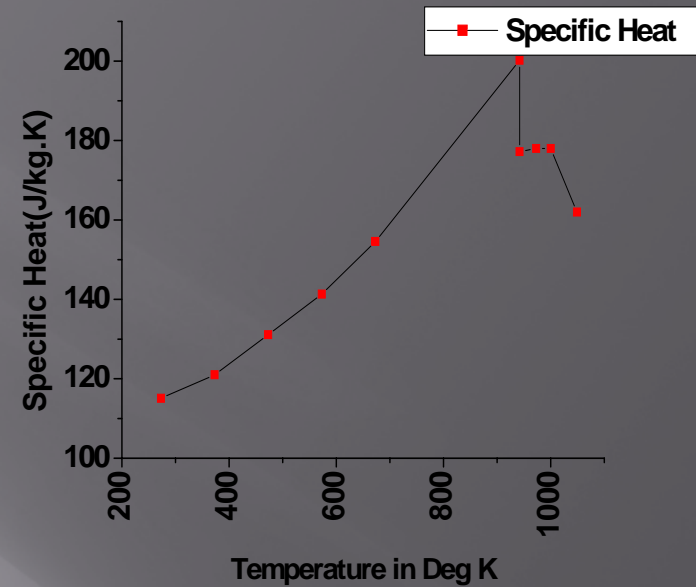


Material properties

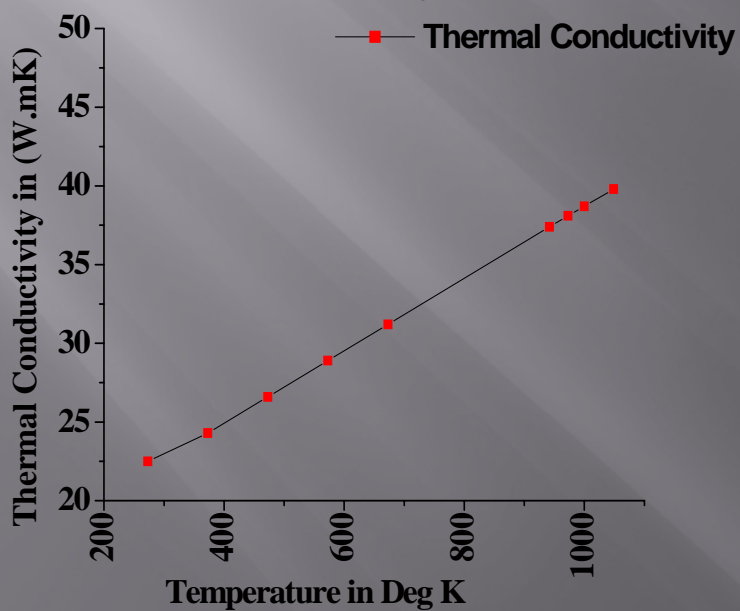
Uranium Density Vs Temperature



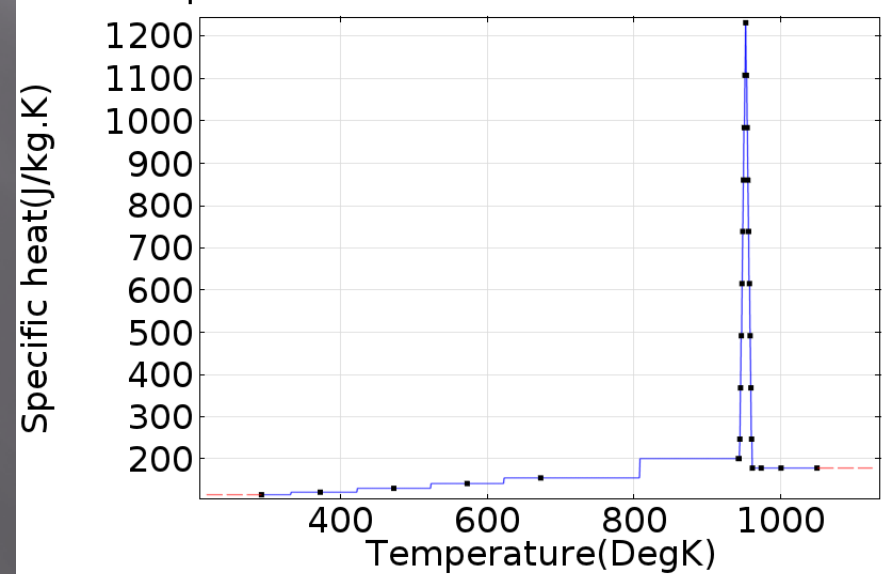
Uranium Specific Heat Vs Temperature



Thermal conductivity Vs Temperature



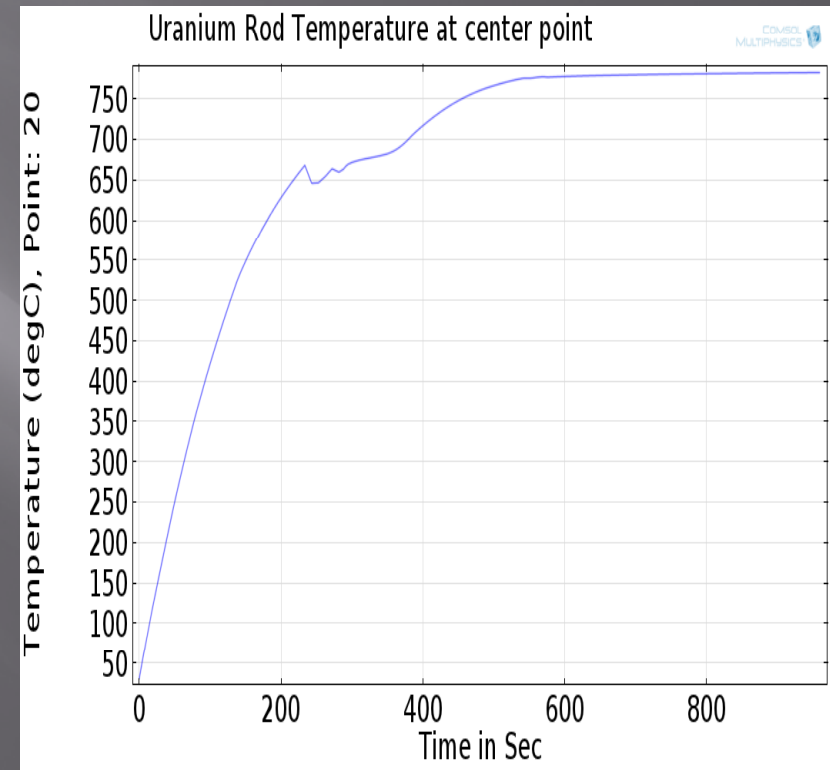
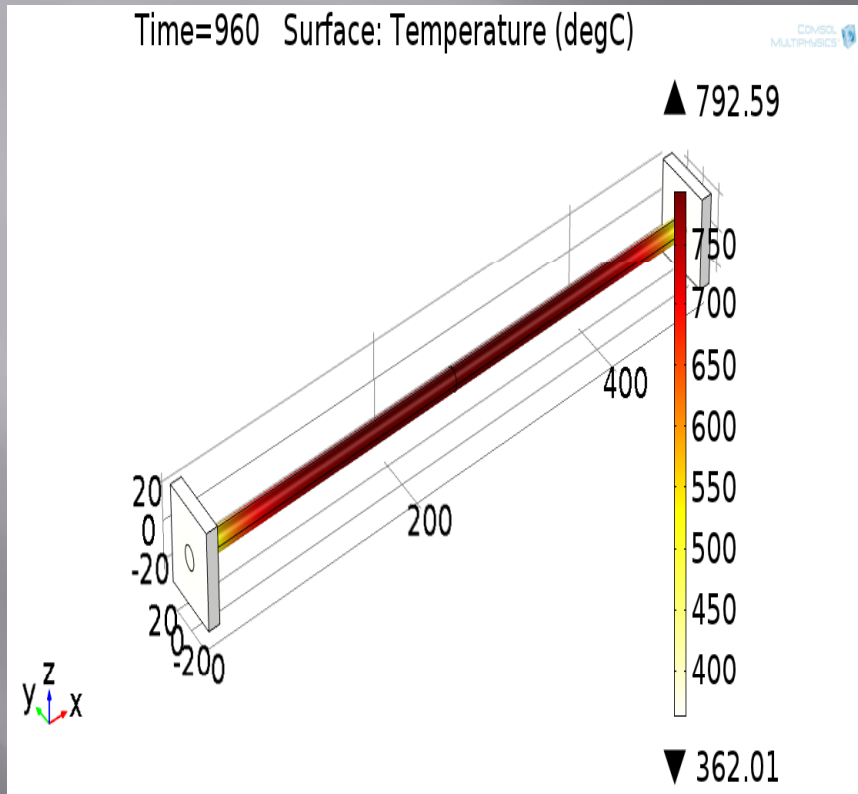
Specific heat of Uranium



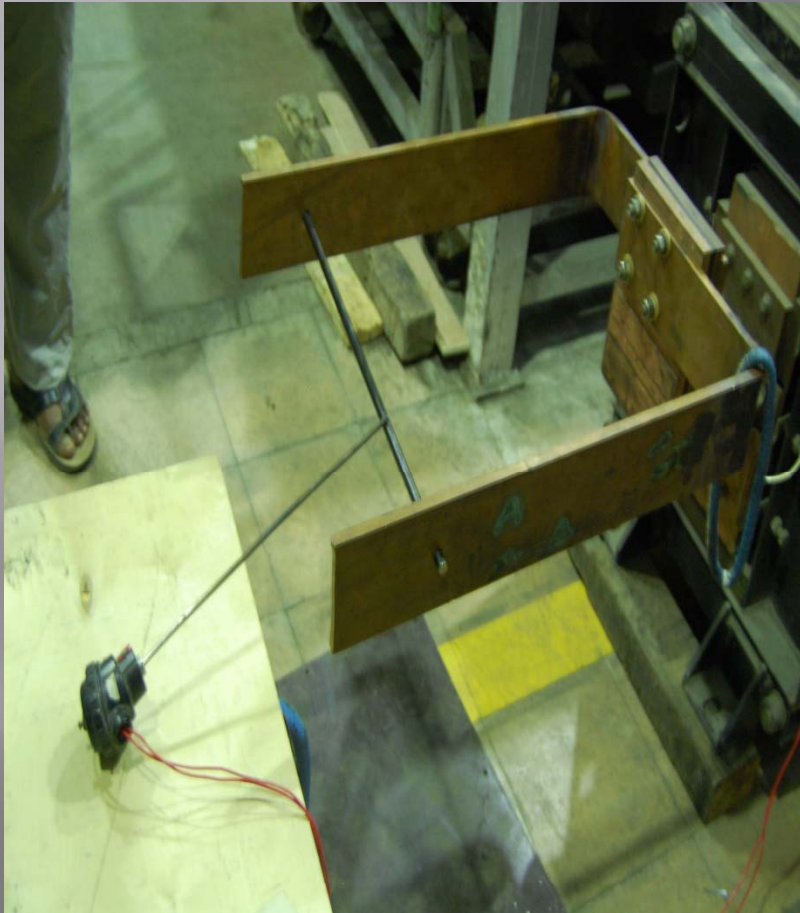
Boundary condition and forcing function

Sr no	Description	Values
1	Convection coefficient (h)	5
2	Emissivity(ϵ)	0.4
3	Initial temperature (Deg K)	304
4	Current	0- 60 Sec:-521 A 60- 960Sec:- 827 A

Simulation Results



Experiment Results

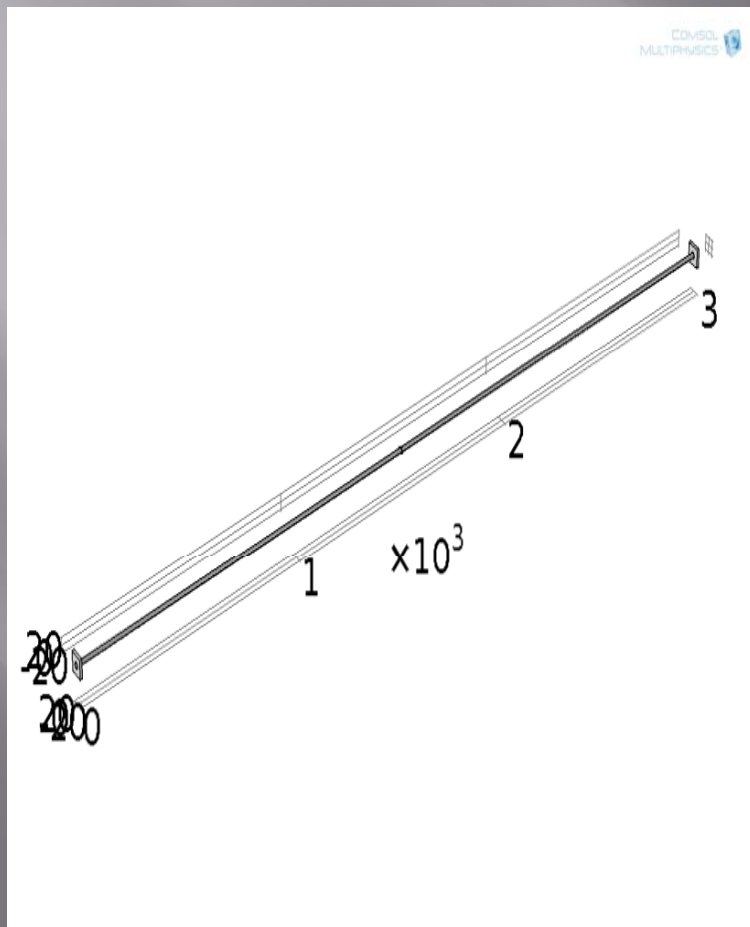


Simulation and Experiment Results

Sr no	Uranium rod 6mm dia X 500 mm L	Uranium rod 50mm dia X 1200 mm L
Simulation results	792 DegC	670 Deg C
Experiment results	810 Deg C	681 Deg C

Simulation on Direct heating of Uranium rod (16 mm dia X3000mm L)

▣ Geometry



Boundary Condition

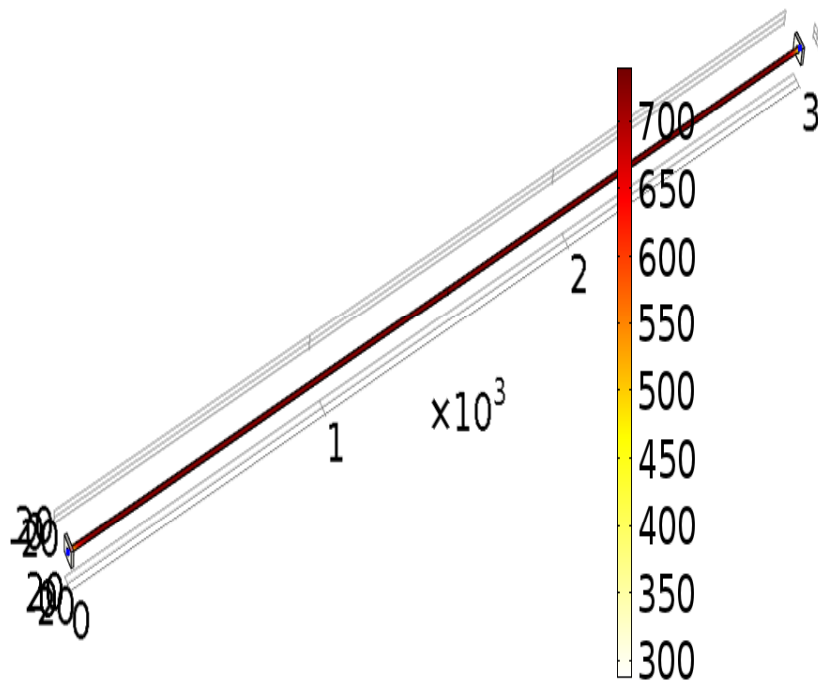
Sr No	Boundary conditions and forcing function	Value
1	Electrical Current	1500 A
2	Heat Transfer	
	Surface to space radiation coefficient	0.4
	Convection heat transfer coefficient	5

Temperature Profile on Uranium rod

Time=90 sec Surface: Temperature (degC)

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▲ 738.83

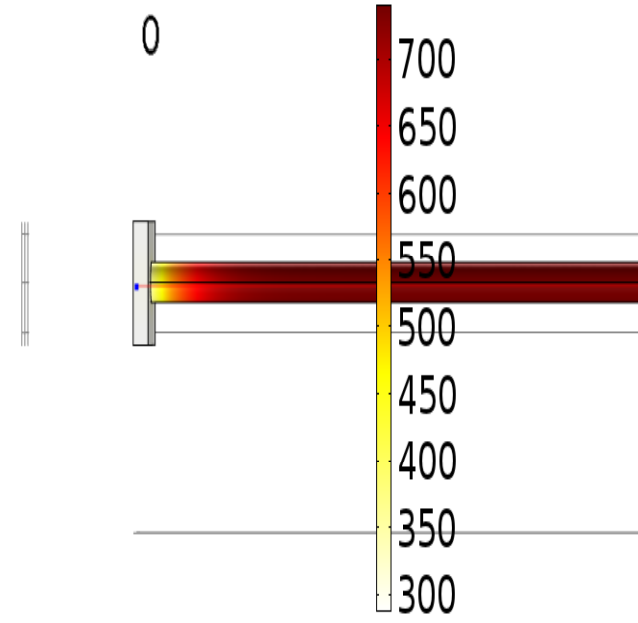


▼ 288.45

Time=90 sec Surface: Temperature (degC)

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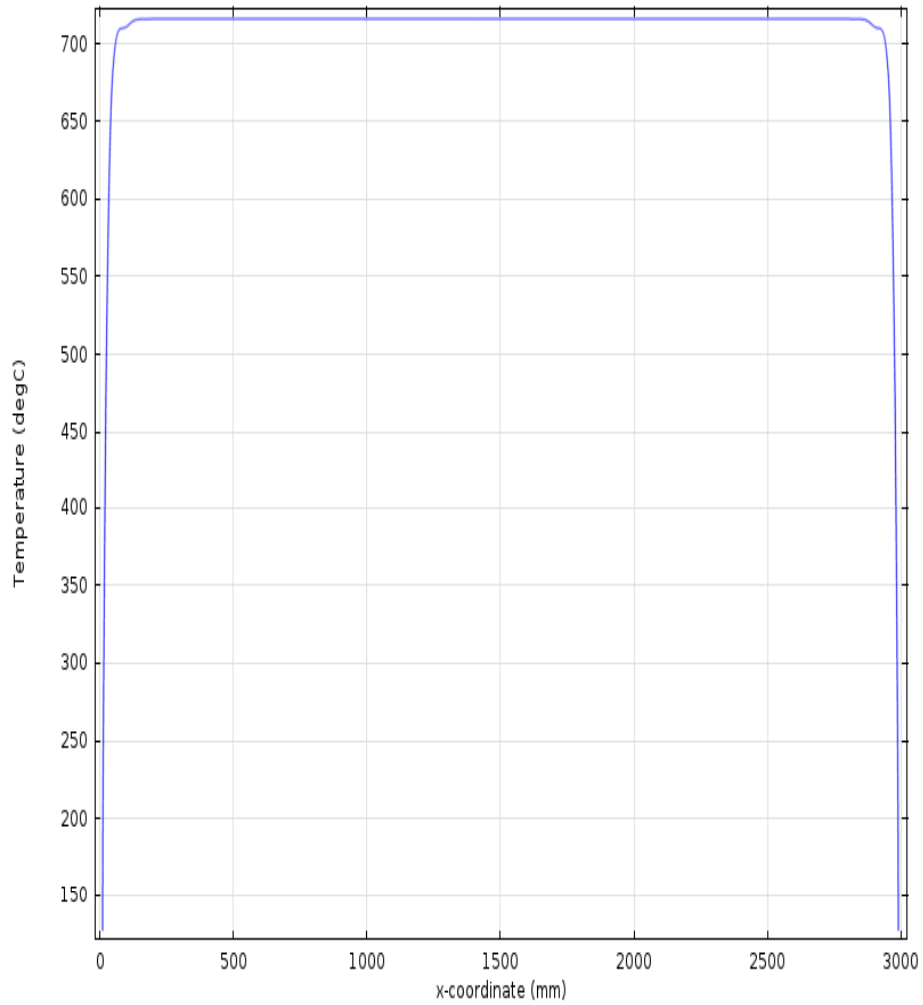
▲ 738.83



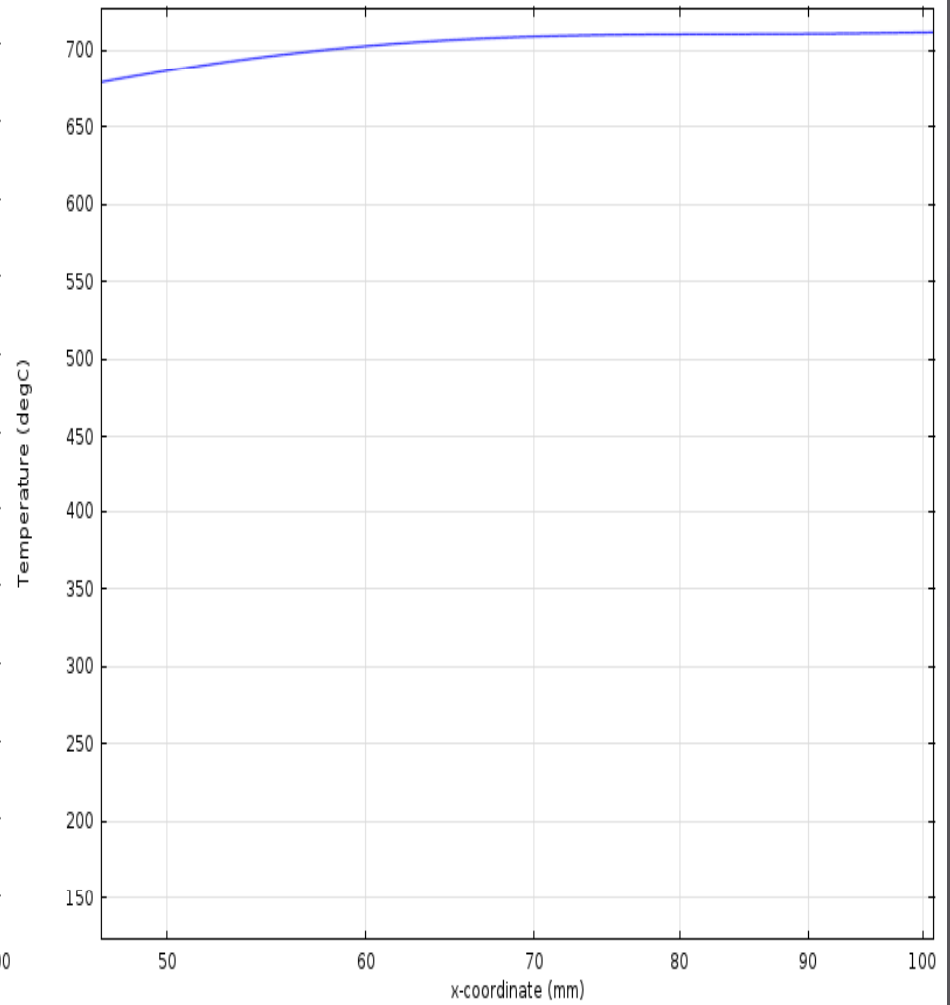
▼ 288.45

Result

Line Graph: Temperature (degC)



Line Graph: Temperature (degC)



Conclusion

- ▣ Direct heating of Uranium rod is possible.
- ▣ Simulation results were very close to experiment results.
- ▣ Direct heating is more efficient compare to indirect heating.
- ▣ No batch wise production is required.

References

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2. Hanyu Ye, El Mehdi boudoudou, Coupled Electro-thermal field simulation in HVDC –cables COMSOL conference in Stuttgart, 2011.
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Thank you