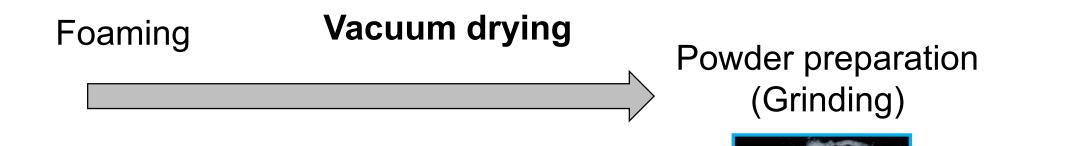
MATHEMATICAL MODEL OF VACUUM FOAM DRYING

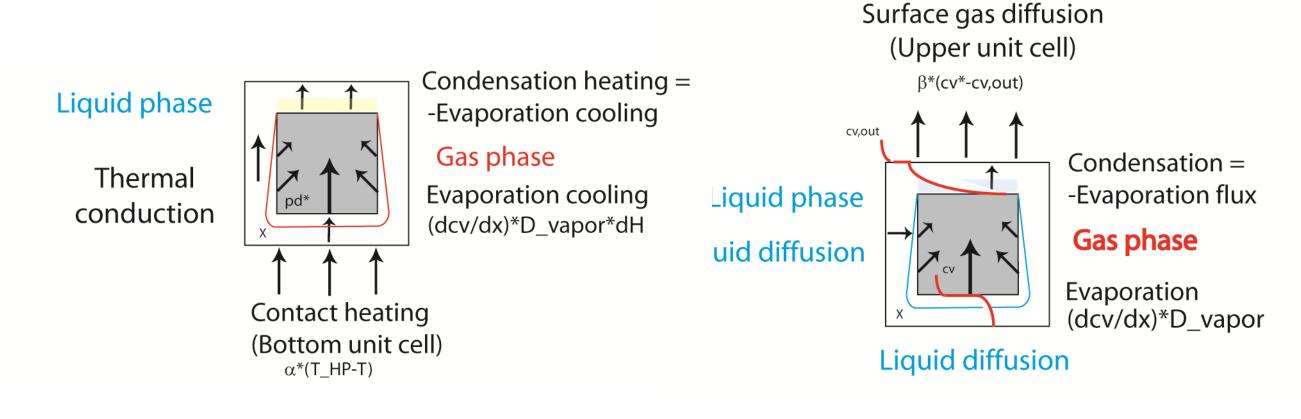
M. Sramek¹, J. Weiss², R. Kohlus¹

1. Universität Hohenheim, Department of Food Process Engineering, Garbenstraße 25, Stuttgart, Germany 2. Universität Hohenheim, Department of Food Physics and Meat Science, Garbenstraße 25, Stuttgart, Germany

Introduction

The presented mathematical model relates closely to the development of a vacuum drying method for highly viscous, sticky and heat and oxygen sensitive materials. The dried materials are closed-pore foams.





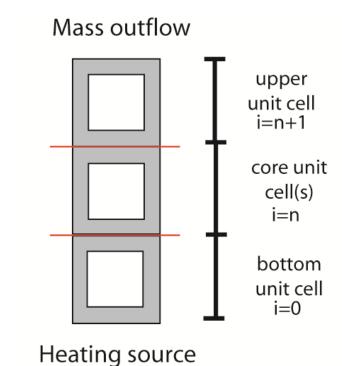
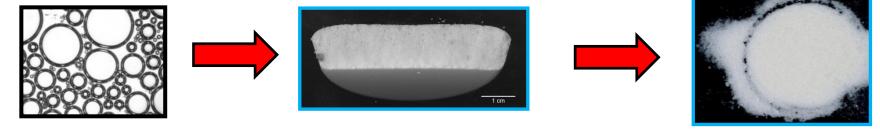


Figure 4. Scheme of heat and mass transfer in unit cell



Free-flowing powder

Figure 1: Process flow vacuum foam drying

The model objectives were to predict local and time dependent temperature and moisture distribution during drying.

Computational Methods

The model is considering foam layer as a repetition of unit cells. The unit cell geometry (fig.1) i.e. the air bubble size *A* and the lamellae thickness *B* are characterizing foam microstructure. The unit cubic cell consists of air and liquid domains, which were approximated by square geometries for simplification. The relationship of air volume fraction ϕ and bubble size/lamellae thickness ratio is given in fig 2. *A*/*B*-ratio

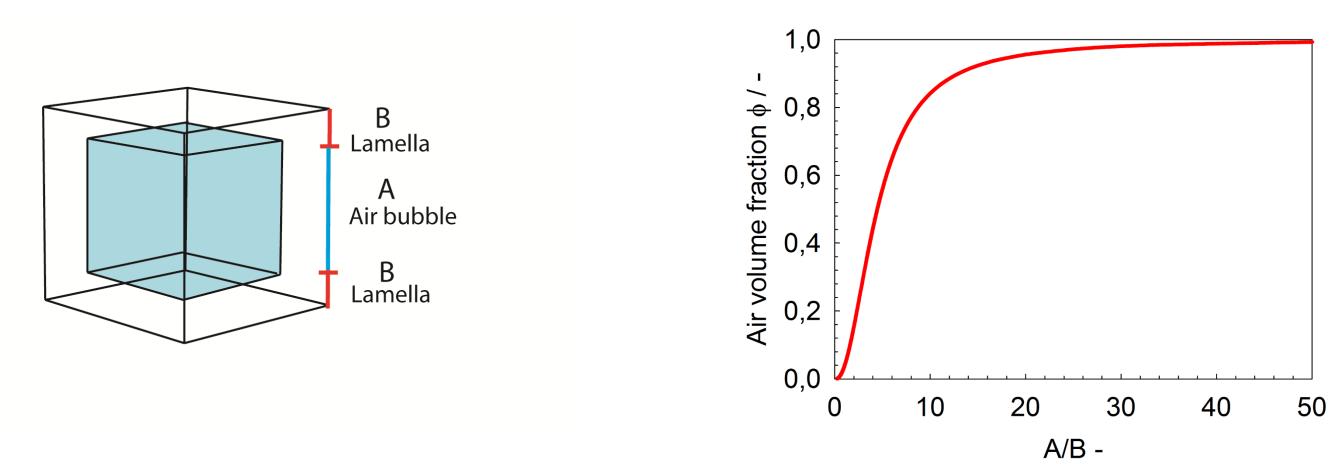
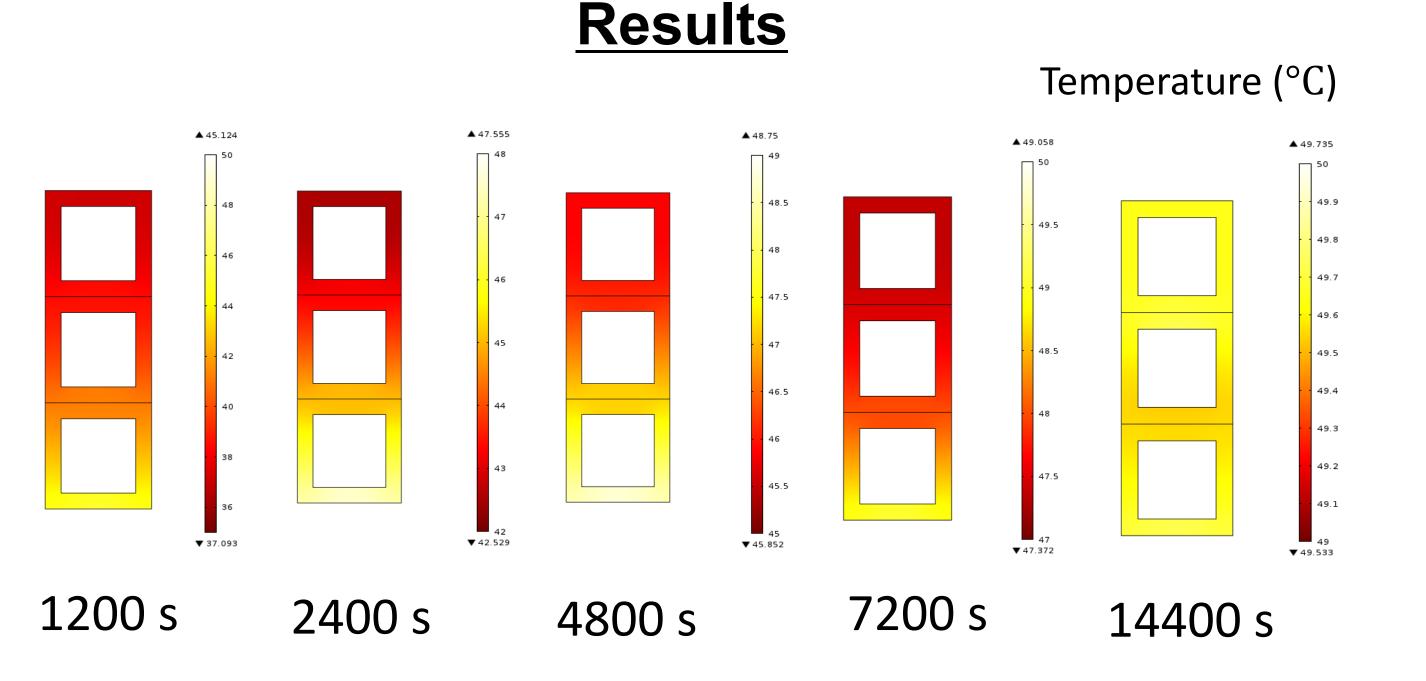


Figure 5. Schematic of multilayer cubic unit cell





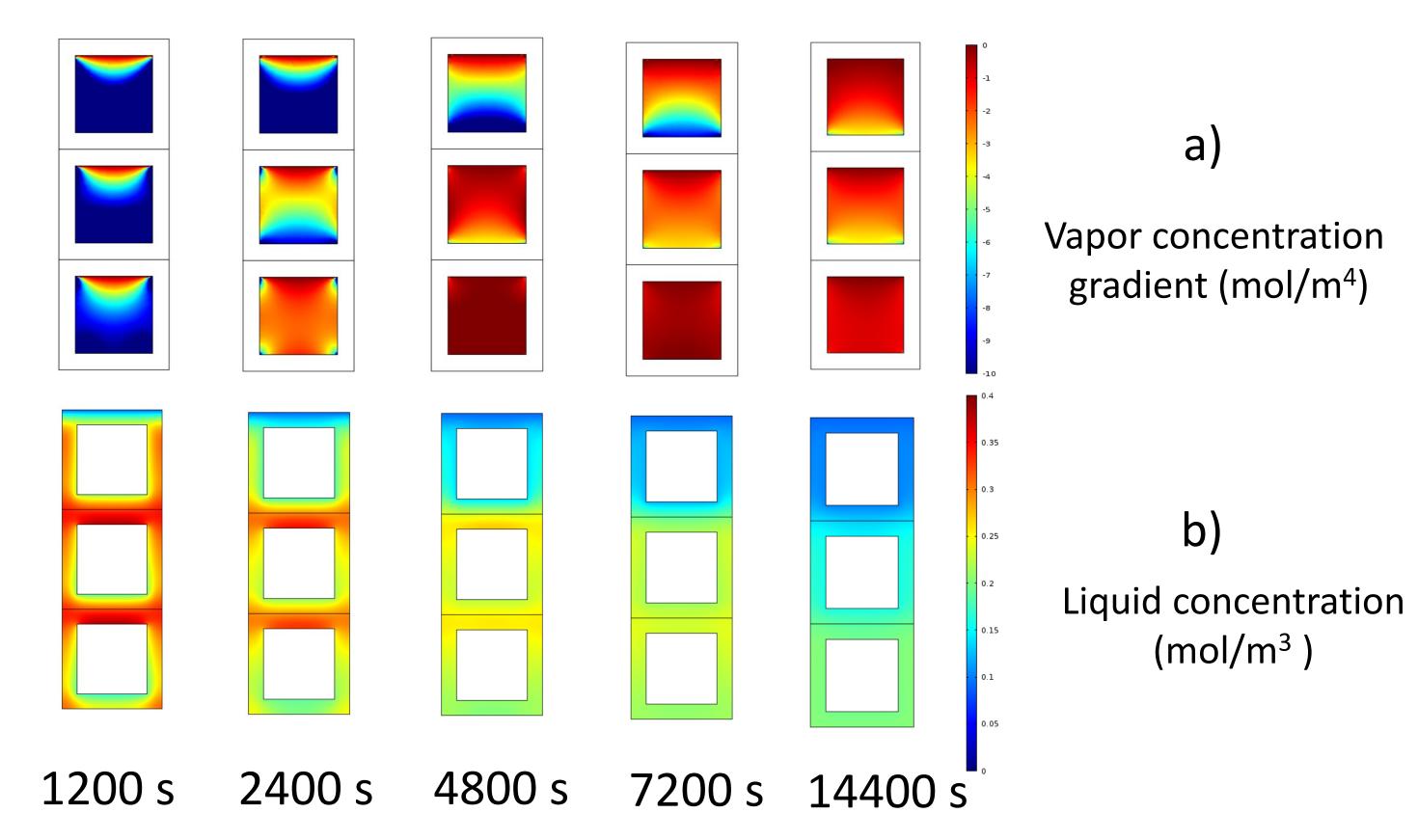


Figure 2. Unit cubic cell

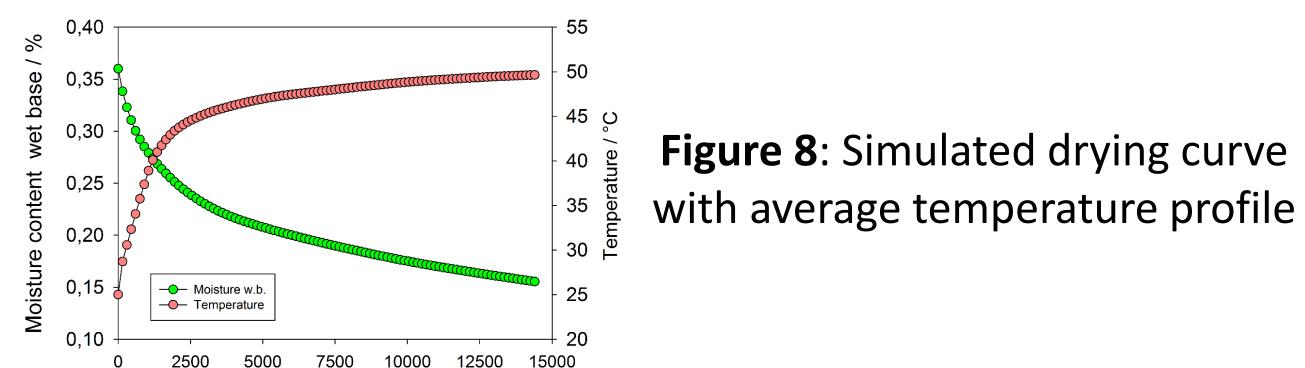
Figure 3. Foam air volume fraction vs. Bubble size / Lamellae thickness ratio A/B

The vacuum foam drying process was modelled in a simultaneous heat and mass transfer. As governing equations Fick law and Fourier law were used. The simulation was solved in a 2D coordinate system.

$$\rho c_p \frac{\partial T}{\partial t} = \nabla \cdot (\lambda \nabla T) \qquad \qquad \frac{\partial w}{\partial t} = \nabla \cdot (D \nabla c)$$

Basic assumptions

The heat transfer is conducted majorly by conduction in foam lamellae and less by evaporation/condensation of vapor in air bubbles. The mass transfer is conducted majorly by vapor diffusion which is driven by vapor partial pressure difference. The partial **Figure 7**: Simulation of mass transfer in 3 layer system: a)development of vapor concentration gradient during drying, b)mass transfer in foam lamellae



pressure gradient arises by spatial temperature difference.

The detailed heat and mass balance and model set-up is given in figure 4 and 5.

Table of main used parameters		Liquid physical properties	Value
		Heat capacity cp Density ρ	3000 [J/(kg*K)] 1170 [kg/m³]
Process parameters	Value	Thermal conductivity λ	0.5 [W/(m*K)]
Heat transfer coefficient λ	50 [W/(m*K)]	Initial water concentration w ₀ Diffusion coefficient DI	20000 [mol/m ³] 1*10 ⁻¹⁰ [m²/s]
Mass transfer coefficient β	0.0001 [m/s]	Vapor physical properties	
Initial temperature T ₀	323 [K]	Diffusion coefficient Dv	1*10 ⁻⁴ [m²/s]
Absolute pressure	100 [mbar]	Enthalpy of evaporation dH	40000 J/mol
Layer thickness	10 [mm]	Initial vapor concentration cv0	2800 [Pa]





- The model provides in simplified form insights to the drying process within a foam microstructure.
- The model allows to estimate discrete heat and mass fluxes during drying in individual unit cell. In each cell conduction, water diffusion, vapor evaporation, condensation can be tracked.
- The model allows a distinction in drying mechanism of foam and non-foamed liquid.

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